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Response to Office Action of April 20, 2005

Amendment to the Specification:

Please replace the paragraph starting with "Japanese Unexamined Patent Publication" beginning on page 1, lines 9-15 with the following amended paragraph:

Japanese Unexamined Patent Publication No. 2003-56463 discloses this type of electric type compressors, which is are integrally provided with the an electric motor, is and are used in a vehicle air conditioning apparatus. In the electric type compressor, a circular stator core for the electric motor is tightly fitted inside of a cylindrical housing by shrink fit and press fit. Since fixing the fixation of the stator core by the tight fit is relatively simple and easy, the associated cost of the electric type compressor is lowered.

Please replace the paragraph starting with "However" beginning on page 1, lines 17-22 and ending on page 2, lines 1-6 with the following amended paragraph:

However, if an <u>aluminum</u> housing <u>made of aluminum</u> is used to reduce the weight of the electric type compressor, since the thermal expansion coefficient of the housing is different from that of the stator core made of iron, <u>a</u> degree of tightness <u>between where</u> the stator core is <u>tightened by and</u> the housing is <u>variedchanges</u> in accordance with <u>a</u> temperature change of the electric type compressor. Note that thermal expansion coefficient of aluminum is larger than that of iron. The interference between the housing and the stator core is predetermined in such a manner that the housing and the stator core are not loosened to <u>with</u> each other even when the temperature of the electric type compressor becomes relatively high. Therefore, on the contrary, when the temperature of the electric type compressor becomes relatively low, the degree of tightness is excessively increased. Thereby, and the housing and/or the stator core generate a crack.

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Please replace the paragraph starting with "The present" beginning on page 2, lines 10-14 with the following amended paragraph:

The present invention is directed to an electric motor and an electric type compressor that prevent generation certain of inconvenience such as a crack even if a housing and a stator core expand or shrink so as to in a tightly fit manner with each other due to a difference in thermal expansion coefficients between the housing and the stator core.

Please replace the paragraph starting with "The present" beginning on page 2, lines 16-21 and ending on page 3, lines 1-6 with the following amended paragraph:

The present invention has following features. An electric motor includes a housing and a circular stator. The housing has an inner circumferential surface. The housing also has with a first predetermined thermal expansion coefficient. The housing further has an elastic part. The stator core is pressed to an inside of the housing by tight fit. The stator core has an outer circumferential surface. The stator core also has with a second predetermined thermal expansion coefficient that is different from the first predetermined thermal expansion coefficient. A void is defined between the inner circumferential surface and the outer circumferential surface so as to prevent the inner and the outer circumferential surfaces from contacting with each other in a circular region. When the housing and the stator core expand or shrink so as to tightly fit with each other due to a differential between the first and the second predetermined thermal expansion coefficients, the an elastic part which corresponds to is located near the void and is elastically deformed.

Please replace the paragraph starting with "An electric" beginning on page 5, lines 4-8 with the following amended paragraph:

An electric type compressor for a vehicle air conditioning apparatus according to a first preferred embodiment of the present invention will now be described with reference to FIGs. 1

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and 2. In FIG. 1, a left side of the FIG. 1 is a front side of the compressor, and a right side thereof is a rear side of the compressor.

Please replace the paragraph starting with "The compressor" beginning on page 5, lines 21-22 and ending on page 6, lines 1-10 with the following amended paragraph:

The compressor housing 11, which is made of the aluminum, is more lightweight than a compressor housing made of iron. The electric type compressor provided with the compressor housing 11 is suitable especially for being installing installed on vehicles in order to improve fuel efficiency. Also, since the first and second housing components 11a and 11b are each manufactured by die casting, in comparison with a case thatto the first and second housing components 11a and 11b are each manufactured by press work, the shape of the compressor housing 11 has a large degree of freedom in forming a certain shape. Therefore, a pin for installing the electric type compressor on the vehicle, which is not shown in the drawings, is easily integrally formed with the compressor housing 11,-. that That is, the first housing component 11a and/or the second housing component 11b integrally form the pin. In this case, the number of parts of the electric type compressor is reduced.

Please replace the paragraph starting with "In the enclosed" beginning on page 7, lines 6-14 with the following amended paragraph:

In the enclosed space 30, a front space 30a and a rear space 30b are defined at the opposite sides of the stator 12 in the direction of the axis L of the stator 12. That is, the front space 30a is defined between the stator 12 and the compression mechanism C, which is located at the front side of the stator 12. Also, the rear space 30b is defined at the rear side of the stator 12. An inlet 18 is formed through the first housing component 11a so as to correspond to be connected to the rear space 30b. The inlet 18 is also connected to a piping in an external refrigerant circuit, that is, or an external piping 24. The inlet 18 serves as a mouth of the electric type compressor.

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Please replace the paragraph starting with "The compression mechanism" beginning on page 7, lines 16-22 and ending on page 8, lines 1-6 with the following amended paragraph:

The compression mechanism C is a scroll type and includes a fixed scroll 20 and a movable scroll 21. The movable scroll 21 is connected to the rotary shaft 13. The movable scroll 21 orbits relative to the fixed scroll 20 in accordance with the rotation of the rotary shaft 13 to compress a refrigerant gas. Therefore, when the compression mechanism C is activated by driving the electric motor M, the refrigerant gas, whose at a relatively low temperature and pressure are relatively low, is drawn from the external refrigerant circuit to the compression mechanism C though the inlet 18, the rear space 30b, the electric motor M and the front space 30a. The temperature and pressure of the refrigerant gas, which has been after drawn into the compression mechanism C, become relatively high by the compressive action compression of the compression mechanism C. The refrigerant gas, whose at a relatively high temperature and pressure are relatively high, is discharged from an outlet 19, which is formed through the second housing component 11b, to the external refrigerant circuit.

Please replace the paragraph starting with "Furthermore," beginning on page 8, lines 8-13 with the following amended paragraph:

Furthermore, the refrigerant gas is circulated through the electric motor M between the external refrigerant circuit and the compression mechanism C. Therefore, the electric motor M is could be cooled by utilizing the refrigerant gas. Especially, since Because the refrigerant gas, whose having a relatively low pressure is relatively low in a refrigerating cycle, is circulated through the electric motor M, the electric motor M is effectively cooled.

Please replace the paragraph starting with "Now, the structure" beginning on page 8, lines 15-22 and ending on page 9, lines 1-5 with the following amended paragraph:

Now, the structure and the operation of the electric motor M will be described. Referring to FIGs. 1 and 2, the stator 12 of the electric motor M includes the coil 15 and a stator core 16 around

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which the coil 15 is wound. The stator core 16 is formed by layering a plurality of silicone steel plates, which is formed by press work, in the direction of the axis L. In other words, <u>a</u> thermal expansion coefficient of the stator core 16 is different from that of the compressor housing 11, which also serves as a housing of the electric motor M. Note that <u>the</u> thermal expansion coefficient of the

aluminum is larger than that of the silicone steel. The stator core 16 includes a circular back yoke 16a

whose center is located on the axis L. The stator core 16 also includes a plurality of teeth 16b that

extends from the inner circumferential surface of the back yoke 16a inward. In the present

embodiment, the number of the teeth 16b is six. In the stator core 16, the coil 15 is intensively

wound around the teeth 16b.

Please replace the paragraph starting with "The stator 12" beginning on page 9, lines 11-12 with the

following amended paragraph:

The stator 12 is fixed toplaced in the first housing component 11a by tightly fitting the stator core 16 to the inner circumferential surface 25a of the circumferential wall 25 of the first housing component 11a. The stator 12 is positioned to the first housing component 11a by contacting the rear end surface of the stator core 16 with a step 25b formed at the rear side of the inner circumferential surface 25a of the circumferential wall 25.

Please replace the paragraph starting with "In the present" beginning on page 9, lines 14-22 and ending on page 10, lines 1-6 with the following amended paragraph:

In the present embodiment, the stator 12 is tightly fitted to the circumferential wall 25 by shrink fit and press fit. Therefore, for example, if since the inner circumferential surface 25a of the circumferential wall 25 and an outer circumferential surface 16c of the stator core 16 contact each other in a circular region or in circumference, since and the thermal expansion coefficient of the circumferential wall 25 is different from that of the stator core 16, a degree of tightness where in the stator core 16 that is tightened by the circumferential wall 25 is varied in accordance with depends on

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 \underline{a} temperature change of the electric type compressor. The interference between the circumferential

wall 25 and the stator core 16 is predetermined in such a manner that the circumferential wall 25 and

the stator core 16 are not loosened to with each other even when the temperature of the electric type

compressor becomes relatively high. Therefore, on the contrary, when the temperature of the electric

type compressor becomes relatively low, the degree of tightness is excessively increased. Thereby,

the circumferential wall 25 and/or the stator core 16 may generate a crack.

Please replace the paragraph starting with "In the present" beginning on page 10, lines 8-11 with the

following amended paragraph:

In the present embodiment, the electric type compressor is structured as follows in such a

manner that the circumferential wall 25 does not become excessively tightly fit around the stator core

16 even when the temperature of the electric type compressor becomes relatively low.

Please replace the paragraph starting with "As shown in Figs. 1 and 2" beginning on page 10, lines

13-20 with the following amended paragraph:

As shown in FIGs. 1 and 2, a void 32 is defined between the inner circumferential surface

25a of the circumferential wall 25 and the outer circumferential surface 16c of the stator core 16.

which are pressed to-against each other by the tight fit, so as to prevent the both circumferential

surfaces 25a and 16c from contacting each other in the circular region, whose center is located on the

axis L. Also, the void 32 extends along the direction of the axis L and interconnects the front space

30a with the rear space 30b in the enclosed space 30. The void 32 serves as a part of a suction gas

passage.

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Please replace the paragraph starting with "As shown in Fig. 2" beginning on page 10, line 22 and ending on page 11, lines 1-7 with the following amended paragraph:

As shown in FIG. 2, the number of the voids 32 is plural and a plurality of the voids 32 is formed around the axis L of the stator core 16. In the present embodiment, the number of the voids 32 is six. Each void 32 is provided by forming a recess 17 in the outer circumferential surface 16c of the stator core 16. That is, each void 32 is a space formed between the associated recess 17 and the circumferential wall 25. A plurality of protrusions 31, which is in the shape of prism, remains in the outer circumferential surface 16c of the stator core 16 by forming a plurality of recesses adjacent to the protrusions 31 in the outer circumferential surface 16c.

Please replace the paragraph starting with "In the outer" beginning on page 11, lines 9-15 with the following amended paragraph:

In the outer circumferential surface 16c of the stator core 16, a distal end surface 31a of each protrusion 31, which is an arched convex surface, is contacted contacts a contact region of with the inner circumferential surface 25a of the circumferential wall 25. The distal end surface 31a of the protrusion 31 of the stator core 16 and the inner circumferential surface 25a of the circumferential wall 25 are contacted with each other in a contact region. A contacting portion 33 includes the distal end surface 31a and the contact region of the inner circumferential surface 25a.

Please replace the paragraph starting with "Each recess 17" beginning on page 12, lines 7-13 with the following amended paragraph:

Each recess 17 has a bottom surface in an arched shape. A region 17a is located at the opposite sides of the protrusion 31 along the bottom surface in a circumferential direction of the stator core 16. In other words, the region 17a adjoins the protrusion 31 of the stator core 16 and exists in a first imaginary cylindrical surface S1, whose center is located on the axis L of the stator core 16. In the middle of the bottom surface of each recess 17 in the circumferential direction of the

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stator core 16, a thinned portion 17b is formed in the shape of a concave surface so as to cave the first imaginary cylindrical surface S1.

Please replace the paragraph starting with "The thinned portion 17b" beginning on page 12, lines 15-22 with the following amended paragraph:

The thinned portion 17b is located near the proximal end of the teeth 16b where a magnetic flux density is relatively lowered in the stator core 16. The object of the thinned portion 17b is mainly to reduce the weight of the stator core 16. <u>However, Ssince</u> the thinned portion 17b is formed in the bottom surface of the recess 17, a cross sectional area of the void 32 in a perpendicular plane to the axis L, through which suction refrigerant gas passes, is <u>also</u> increased. Therefore, efficiency of intake of the compression mechanism C and cooling efficiency of the electric motor M are improved.

Please replace the paragraph starting with "A described above," beginning on page 13, lines 1-18 with the following amended paragraph:

As described above, the inner circumferential surface 25a of the circumferential wall 25 is contacted with contacts the outer circumferential surface 16c of the stator core 16 in the contact region. That is, the inner circumferential surface 25a of the circumferential wall 25 is contacted with contacts the distal end surface 31a of the protrusion 31 in the contacting portion 33. The contact region exists in a second imaginary cylindrical surface S2, whose center is also located on the axis L. The second imaginary cylindrical surface S2 has the same length as the stator core 16 in the direction of the axis L. The radial differential between the second imaginary cylindrical surface S2 and the first imaginary cylindrical surface S1, that is, the height of the protrusion 31 that protrudes from the first imaginary cylindrical surface S1, is predetermined in such a manner that a ratio of the radial differential to the radius of the second imaginary cylindrical surface S2 is approximately 5/1000 to 15/1000. The electric type compressor according to the present embodiment is set in such a manner that the radius of the second imaginary cylindrical surface S2 is approximately 50 mm. Therefore,

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the height of the protrusion 31 is approximately 0.25 mm to 0.75 mm. Note that the height of the

protrusion 31 is exaggeratedly shown in FIGs. 1 and 2.

Please replace the paragraph starting with "(1) The void 32" beginning on page 14, lines 13-22

and ending on page 15, lines 1-6 with the following amended paragraph:

(1) The void 32 is defined between the inner circumferential surface 25a of the circumferential

wall 25 of the first housing component 11a and the outer circumferential surface 16c of the stator

core 16 so as to prevent the both circumferential surfaces 25a and 16c from contacting with each

other in the circular region. Therefore, when the temperature of the electric type compressor becomes

relatively low, if the circumferential wall 25 \underline{is} made of the aluminum and the stator core 16 \underline{is} made

of silicone steel shrink so as to tightly fit each other due to the difference in thermal expansion

coefficient between the circumferential wall 25 and the stator core 16, an elastic part 25d of the

circumferential wall 25 which corresponds to is located near the void 32 is elastically deformed

toward the void 32 as-like a leaf spring is done. The elastic part 25d has a curved tabular shape. The

elastic deformation of the elastic part 25d absorbs the difference in shrinkage between the

circumferential wall 25 and the stator core 16, thereby preventing the circumferential wall 25 from

excessively tightly fitting the stator core 16. Thus, the generation of the crack of the circumferential

wall 25 and/or the stator core 16 is prevented. As a result, the durability of the electric type

compressor is improved.

Please replace the paragraph starting with "(2) A plurality of" beginning on page 15, lines 8-21

with the following amended paragraph:

(2) A plurality of the voids 32 is provided around the axis L of the stator core 16. That is, in the

circumferential wall 25 of the compressor housing 11, a plurality of the elastic parts 25d is arranged

around the axis L of the stator core 16. Therefore, when the temperature of the electric type

compressor becomes relatively low, if the circumferential wall 25 and the stator core 16 shrink so as

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to tightly fit each other, the circumferential wall 25 is elastically deformed so as to share between a pluralityequally at each of the elastic parts 25d. Therefore, for example, in comparison with a case that the number of the voids 32 is only one, namely, a case that the circumferential wall 25 is intensively but elastically deformed at one elastic part 25d, a plurality of the voids 32 securely prevents the circumferential wall 25 from excessively tight fitting the stator core 16. Furthermore, damage is also prevented of from being made to the circumferential wall 25 or the compressor housing 11, which is caused by the excessive deformation of a part of the circumferential wall 25 or one elastic part 25d, is also prevented.

Please replace the paragraph starting with "(3) The number of" beginning on page 16, lines 1-12 with the following amended paragraph:

The number of the voids 32, which is provided around the axis L of the stator core 16, is three or more than three. That is, the circumferential walls 25 of the compressor housing 11 and the stator core 16 are contacted with each other around the axis L of the stator core 16 at at least three spots or more than three spots. Therefore, the number of the contacting portions 33, where the stator core 16 is supported by the circumferential wall 25, is at least three-or more than three, and such contacting portions 33 are arranged around the axis L of the stator core 16. Since the stator core 16 is supported by the circumferential wall 25 at at least three spots or more than three spots, for example, in comparison to two of with a case that the number of the voids 32 is two, namely, a case that the number with two of the contacting portions 33 between the circumferential wall 25 and the stator core 16 is two around the axis L, the stator core 16 is more steadily supported by the circumferential wall 25.

Please replace the paragraph starting with "Accordingly, when" beginning on page 16, lines 14-19 with the following amended paragraph:

Accordingly, when the electric type compressor is manufactured, the axis L of the stator core16 and the axis L of the circumferential wall 25 are is easily conformed for the stator core16

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and the circumferential wall 25to each other. For example, when the rotary shaft 13 is installed on in the compressor housing 11 through the front bearing 22 and the rear bearing 23, the rotor 14, which is installed on the rotary shaft 13, is hardly interfered with the stator core 16. Thus, the electric type compressor is easily manufactured.

Please replace the paragraph starting with "(4) The contacting portions" beginning on page 16, lines 21-22 and ending on page 17, lines 1-8 with the following amended paragraph:

(4) The contacting portions 33 between the circumferential wall 25 of the compressor housing 11 and the stator core16 are arranged at intervals of an equal angle around the axis L. Therefore, in comparison with a case that the contacting portions 33 are arranged at intervals of an unequal angle around the axis L, the stator core 16 is <u>more</u> steadily supported by the circumferential wall 25. Furthermore, even if the circumferential wall 25 and the stator core 16 shrink so as to tightly fit each other due to <u>a</u> thermal effect, each elastic part 25d is equally <u>and</u> elastically deformed. Thereby, damage <u>of to</u> the circumferential wall 25, which is caused by the excessive deformation of a part of the elastic parts 25d or one elastic part 25d, is securely prevented.

Please replace the paragraph starting with "(5) The void 32" beginning on page 17, lines 10-14 with the following amended paragraph:

(5) The void 32 is provided by forming the recess 17 in the outer circumferential surface 16c of the stator core 16. Therefore, if the present first embodiment of the present invention is to be applied to an prior art electric type compressor-according to a prior art, the void 32 is simply formed by changing a part of the shape of an existing press die for manufacturing a stator core.

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Please replace the paragraph starting with "(6) The height of" beginning on page 17, lines 16-22 and ending on page 18, line 1 with the following amended paragraph:

The height of the protrusion 31 that extends from the first imaginary cylindrical surface S1 is set-determined in such a manner that a ratio of the height of the protrusion 31 to the radius of the second imaginary cylindrical surface S2 is approximately 5/1000 to 15/1000. Therefore, increase of the increased size of the electric type compressor and deterioration of the deteriorated efficiency of the electric motor M are prevented. In addition, in the circumferential wall 25, the elastic part 25d is securely elastically deformed. Thus, the prevention is compatible with the elastic deformation at a relatively high level.

Please replace the paragraph starting with "In other words," beginning on page 18, lines 3-19 with the following amended paragraph:

In other words, in order to prevent the deterioration of the efficiency of the electric motor M while preventing and the increase of the diameter of the stator core 16, which increases the size of the electric type compressor, a radial differential needs to be reduced between the second imaginary cylindrical surface S1 requires reducing. Thereby Since, the depth of the recess 17, which is a cause of magnetic saturation, requires reducing the depth needs to be reduced. Specifically, the depth of the recess 17 other than the thinned portion 17b, or the depth of the region 17a, requires reducing needs to be reduced. On the other hand, in order to securely and elastically deform the elastic part 25d of the circumferential wall 25, the radial differential or the height of the protrusion 31 that protrudes from the first imaginary cylindrical surface S1 requires increasing. Thereby, a space for permitting the elastic deformation of the circumferential wall 25 requires to securing secure a predetermined volume. In other words, the depth of the recess 17 requires to securing secure a predetermined length. To fulfill the suitable balance between the reduction and the securement of in the depth of the recess 17, as described above, the ratio of the height of the protrusion 31 to the radius of the second imaginary cylindrical surface S2 is preferably

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approximately in a range of 5/1000 to 15/1000 or 0.5 to 1.5%.

Please replace the paragraph starting with "(7) In the second imaginary" beginning on page 18, lines 21-22 and ending on page 19, lines 1-18 with the following amended paragraph:

(7)In the second imaginary cylindrical surface S2, as descried above, the contact region where the inner circumferential surface 25a of the circumferential wall 25 contacts the outer circumferential surface 16c of the stator core 16 has the first predetermined area. Also, the non-contact region where the inner circumferential surface 25a of the circumferential wall 25 does not contact the outer circumferential surface 16c of the stator core 16 has the second predetermined area. The void 32 is formed between the inner circumferential surface 25a of the circumferential wall 25 and the outer circumferential surface 16c of the stator core 16 in such a manner that the first predetermined area becomes smaller than the second predetermined area. Thus, since the first predetermined area of the contact region is set to be relatively small, in the circumferential wall 25, the elastic part 25d is secured in a relatively large region of the circumferential wall 25. Therefore, the elastic deformation of the elastic part 25d is effectively performed. Thereby, excessively tightening the stator core 16 is securely prevented. As a result, generation of inconvenience such as the a crack is securely prevented. Specifically, in on the second imaginary cylindrical surface S2, setting the ratio of the first predetermined area to the total area of the first predetermined area and the second predetermined area is set to be 30% or less than 30% in order to securely prevents the circumferential wall 25 from excessively tightening the stator core 16.

Please replace the paragraph starting with "(8) The inlet 18" beginning on page 19, lines 20-22 and ending on page 20, lines 1-3 with the following amended paragraph:

(8) The inlet 18 and the compression mechanism C are in communication with a suction refrigerant gas passage. The void 32 forms a part of the suction refrigerant gas passage. Therefore, the electric motor M is effectively cooled by suction refrigerant gas <u>in-at a relatively</u> low

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temperature, which passes through the void 32. Thereby, <u>the</u> deterioration <u>of thein</u> efficiency of the electric type compressor <u>is prevented eaused by the from raise raising of</u> the temperature of the electric motor M-is prevented.

Please replace the paragraph starting with "(9) The void 32" beginning on page 20, lines 5-12 with the following amended paragraph:

(9) The void 32 serves as a part of the suction refrigerant gas passage mainly because of in the thinned portion 17b formed in the stator core 16, which occupies a relatively large part of the cross sectional area of the void 32. If the void 32 is provided by forming a recess only at the side of the inner circumferential surface 25a of the circumferential wall 25, in order to secure the cross sectional area for passing the refrigerant gas, which corresponds to the thinned portion 17b, the diameter of the circumferential wall 25 requires needs to be increasing increased in order to secure the cross sectional area for passing the refrigerant gas, which corresponds to the thinned portion 17b. Thereby, the size of the electric type compressor is also increased.

Please replace the paragraph starting with "However," beginning on page 20, lines 16-22 and ending on page 21, lines 1-6 with the following amended paragraph:

However, in the present embodiment where the void 32 is provided by forming the recess 17 in the outer circumferential surface 16c of the stator core 16, the thinned portion 17b is formed so as to correspond to the teeth 16b of the stator core 16. In other words, the thinned portion 17b is formed so as not to generate the magnetic saturation. Thereby, the thinned portion 17b does not increase the diameter of the stator core 16. Namely, the size of the electric type compressor is not increased. Meanwhile, since the stator core 16 is structured in such a manner that the coil 15 is intensively wounded around the teeth 16b, even if the thinned portion 17b is formed so as to correspond to the teeth 16b of the stator core 16, the magnetic saturation does is not generated. However, if the stator core 16 is structured in such a manner that the coil 15 is distributively wounded around the teeth 16b,

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the magnetic saturation may <u>be generated</u> by forming the thinned portion 17b in the stator core 16. Therefore, in order to prevent the generation of the magnetic saturation, the diameter of the stator core 16 requires needs to be <u>increasing increased</u> by a radial length of the thinned portion 17b.

Please replace the paragraph starting with "That is," beginning on page 21, lines 8-13 with the following amended paragraph:

That is, in the electric type compressor provided with the electric motor M where the coil 15 is intensively wounded around the teeth 16b, the void 32 is provided by forming the recess 17 in the outer circumferential surface 16c of the stator core 16. Thereby, the void 32 also serves as a part of the suction refrigerant gas passage without increasing the size of the electric type compressor.

Please replace the paragraph starting with "An electric type" beginning on page 21, lines 15-22 and ending on page 22, lines 1-6 with the following amended paragraph:

An electric type compressor for a vehicle air conditioning apparatus according to a second preferred embodiment of the present invention will now be described with reference to FIG. 3. In the second embodiment, only different aspects from the first embodiment are described. Identical reference numerals to the first embodiment are applied to <u>substantially</u> the same or <u>corresponding</u> members in the second embodiment, and <u>the overlapped overlapping</u> description is omitted. In the <u>present second</u> embodiment, in comparison with the first embodiment, the teeth 16b of the stator core 16 of the electric motor M are relatively compact and the number of the teeth 16b is increased. Specifically, in the present embodiment, the number of the teeth 16b is twenty-four. In the present embodiment, the stator core 16 is structured in such a manner that the coil 15 is distributively wounded around the teeth 16b of the stator core 16. Such structured electric motor M that the coil 15 is distributively wounded around the teeth 16b is more noiseless than the electric motor M, where the coil 15 is intensively wounded around the teeth 16b.

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Please replace the paragraph starting with "Also, in the present" beginning on page 22, lines 8-17with the following amended paragraph:

Also, in the present embodiment, the void 32 is provided not by forming a recess 36 in the outer circumferential surface 16c of the stator core 16 but by forming the recess 36 in the inner circumferential surface 25a of the circumferential wall 25. The number of the recesses 36 is plural, and the recesses 36 are formed around the axis L at intervals of an equal angle. In the present embodiment, the number of the recesses 36 is six. Each recess 36 extends along the direction of the axis L in the enclosed space 30 of the compressor housing 11 and is formed so as to become larger than the total length in the direction of the axis L of the stator core 16. Thereby, the recess 36 interconnects the front space 30a with the rear space 30b.

Please replace the paragraph starting with "A plurality" beginning on page 22, lines 19-22 and ending on page 23, lines 1-8 with the following amended paragraph:

A plurality of protrusions 37 remains in the inner circumferential surface 25a of the circumferential wall 25 by after forming a plurality of the recesses 36 in the inner circumferential surface 25a. A distal end surface 37a of each protrusion 37, which is in the shape of an arched concave surface, is contacted with a cylindrical outer surface of the stator core 16 or the outer circumferential surface 16c in a contact region. The contacting portion 33 includes the distal end surface 37a and the contact region of the outer circumferential surface 16c. A bottom surface 36a of each recess 36 is as a whole in the shape of a curved concave surface. Therefore, the inner circumferential surface 25a of the circumferential wall 25 is a waved shaped form in the circumferential direction of the stator core 16, and the elastic part 25d of the circumferential wall 25 is thinner than a other parts of the circumferential wall 25, which corresponds to the contacting portion 33.

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Please replace the paragraph starting with "In the second embodiment" beginning on page 23, lines 10-11 with the following amended paragraph:

In the second embodiment, the above-described effects $(1) \sim (4)$, (7), and (8) are substantially obtained. In addition, the following effects are also obtained.

Please replace the paragraph starting with "(10) The void 32" beginning on page 23, lines 13-18 with the following amended paragraph:

(10) The void 32 is provided by forming the recess 36 in the inner circumferential surface 25a of the circumferential wall 25 of the first housing component 11a. Therefore, when the present embodiment is applied to <u>prior art</u> the electric type compressors according to the prior art, the void 32 is simply provided by changing a part of the shape of an existing die for manufacturing the first housing component 11a.

Please replace the paragraph starting with "(11) In the present embodiment" beginning on page 23, lines 20-22 and ending on page 24, lines 1-10 with the following amended paragraph:

(11) In the present embodiment where the stator core 16 is structured in such a manner that the coil 15 is distributively wounded around the teeth 16b, if a recess similar to the recess 17 of the first embodiment is formed in the outer circumferential surface 16c of the stator core 16, the magnetic saturation may be generated. Therefore, in order to prevent the generation of the magnetic saturation, the diameter of the stator core 16 is requires required to increasing increase by the length of the recess 17 in the radial direction of the stator core 16 or the depth of the recess 17. In the present embodiment, however, since the void 32 is provided by forming the recess 36 in the inner circumferential surface 25a of the circumferential wall 25, for example, in comparison with a case that to the void 32 is provided by forming the recess 17 in the outer circumferential surface 16c of the stator core 16, the diameter of the stator core 16 is more reduced. That is, the size of the electric motor M is also reduced.

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Please replace the paragraphs starting with "An electric type" beginning on page 24, lines 12-19 and starting with "That is," beginning on page 24, lines 21-22 and ending on page 25, lines 1-3 with the following amended paragraph:

An electric type compressor for a vehicle air conditioning apparatus according to a third preferred embodiment of the present invention will now be described with reference to FIG. 4. In the third embodiment, only different aspects different from the second embodiment are described. Identical reference numerals to the second embodiment are applied to substantially the same of corresponding members in the third embodiment, and overlapped overlapping description is omitted. In the present embodiment, the number of the voids 32, which are provided around the axis L, is three. That is, the circumferential wall 25 of the compressor housing 11 and the stator core 16 are contacted with each other at three spots around the axis L of the stator core 16. Therefore, there are the three contacting portions 33 where the stator core 16 is supported by the circumferential wall 25 around the axis L of the stator core 16.

That is, the circumferential wall 25 of the compressor housing 11 and the stator core 16 are contacted with each other at three spots around the axis L of the stator core 16. Therefore, the number of the contacting portions 33 where the stator core 16 is supported by the circumferential wall 25 around the axis L of the stator core 16 is three.

Please replace the paragraph starting with "In the present embodiment" beginning on page 25, lines 5-16 with the following amended paragraph:

In the present embodiment, the recess 36, which is formed in the inner circumferential surface 25a of the circumferential wall 25, is formed by expanding the elastic part 25d outwardly in the radial direction of the circumferential wall 25. Therefore, an outer circumferential surface 25c of the circumferential wall 25 is has a waved-shaped form in the circumferential direction of the stator core 16 that is similarly to the inner circumferential surface 25a, and but is different from an outer circumferential surface of the circumferential wall 25 of the above-described second embodiment,

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which forms a circumferential surface. That is, the circumferential wall 25 is has a waved-shaped form in the circumferential direction of the stator core 16 so as to maintain a substantially uniform thickness, and is formed in such a manner that tThe thickness of the part of the circumferential wall 25, which corresponds to the contacting portion 33, becomes is equal to the thickness of the elastic part 25d.

Please replace the paragraphs starting with "An electric type" beginning on page 25, lines 18-22, ending on page 26, lines 1-3 and starting with "That is," beginning on page 25, lines 5-9 with the following amended paragraph:

An electric type compressor for a vehicle air conditioning apparatus according to a fourth preferred embodiment of the present invention will now be described with reference to FIG. 5. In the fourth embodiment, only different aspects different from the third embodiment are described. Identical reference numerals to the third embodiment are applied to substantially the same of corresponding members in the fourth embodiment, and overlapped overlapping description is omitted. In the present embodiment, the number of the voids 32, which are provided around the axis L, is four. That is, the circumferential wall 25 of the compressor housing 11 and the stator core 16 contact with each other at four spots around the axis L of the stator core 16. Therefore, there are four contacting portions 33 where the stator core 16 is supported by the circumferential wall 25 around the axis L of the stator core 16.

That is, the circumferential wall 25 of the compressor housing 11 and the stator core 16 are contacted with each other at four spots around the axis L of the stator core 16. Therefore, the number of the contacting portions 33 where the stator core 16 is supported by the circumferential wall 25 around the axis L of the stator core 16 is four.

Please replace the paragraph starting with "An electric type" beginning on page 26, lines 11-17, and starting with "That is," beginning on page 26, lines 19-22 with the following amended paragraph:

An electric type compressor for a vehicle air conditioning apparatus according to a fifth preferred embodiment of the present invention will now be described with reference to FIG. 6. In the

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fifth embodiment, only different aspects different from the third embodiment are described. Identical reference numerals to the third embodiment are applied to <u>substantially</u> the same or <u>corresponding members</u> in the fifth embodiment, and <u>overlapped overlapping</u> description is omitted. In the present embodiment, the number of the voids 32, which are provided around the axis L, is five. <u>That is, the circumferential wall 25 of the compressor housing 11 and the stator core 16 contact with each other at five spots around the axis L of the stator core 16. Therefore, there are five contacting portions 33 where the stator core 16 is supported by the circumferential wall 25 around the axis L of the stator core 16.</u>

That is, the circumferential wall 25 of the compressor housing 11 and the stator core16 are contacted with each other at five spots around the axis L of the stator core 16. Therefore, the number of the contacting portions 33 where the stator core 16 is supported by the circumferential wall 25 around the axis L of the stator core 16 is five.

Please replace the paragraph starting with "(12) The recess 36" beginning on page 27, lines 7-19 with the following amended paragraph:

(12) The recess 36 of the inner circumferential surface 25a of the circumferential wall 25 is formed by expanding the elastic part 25d of the circumferential wall 25 outwardly in the radial direction of the stator core 16. Therefore, the circumferential wall 25 is formed in the shape of a wave in the circumferential direction of the stator core 16 so as to maintain a substantially uniform thickness by the outward expansion of the elastic part 25d in the radial direction of the stator core 16. Thereby, for example, in comparison with a case thatto second preferred embodiment having the recess 36 is formed in the inner circumferential surface 25a of the circumferential wall 25 in such a manner that the whose elastic part 25d becomes thinner than the part of the circumferential wall 25, which corresponds to the contacting portion 33, rigidity of the circumferential wall 25, that is, rigidity and of the first housing component 11a is enhanced. Thus, durability of the electric type

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compressor is improved.

Please replace the paragraph starting with "(13) In the circumferential" beginning on page 27, lines 21-22 and ending on page 28, lines 1-4 with the following amended paragraph:

(13) In the circumferential wall 25, the number of spots where the elastic part 25d is expanded outwardly in the radial direction of the stator core 16 around the axis L is five or less than five. Therefore, even if the circumferential wall 25 and the stator core 16 shrink so as to tightly fit each other due to thermal effects, such a small number of spots prevents the circumferential wall 25 from excessively tightly fitting the stator core 16.

Please replace the paragraph starting with "That is," beginning on page 28, lines 6-16 with the following amended paragraph:

That is, when the circumferential wall 25 is expanded outwardly, in comparison with a ease that preferred embodiment having the circumferential wall 25 that is not expanded outwardly, the rigidity of the circumferential wall 25 is lowered. Besides, for example, if the number of spots where the elastic parts 25d or the voids 32 is provided around the axis L of the stator core 16 is at least six or more than six, and if six or more than six in the corresponding plurality of elastic parts 25d are is respectively expanded outwardly in the radial direction of the stator core 16, the rigidity of the circumferential wall 25 is excessively enhanced. At this time, each elastic part 25d is hardly elastically deformed in an elastic manner. Therefore, if the circumferential wall 25 and the stator core 16 shrink so as to tightly fit each other due to thermal effects, the circumferential wall 25 excessively tightly fit the stator core 16 because of such a great number of spots.

Please replace the paragraph starting with "An electric type" beginning on page 28, lines 18-22 and ending on page 29, lines 1-2 with the following amended paragraph:

An electric type compressor for a vehicle air conditioning apparatus according to a sixth preferred embodiment of the present invention will now be described with reference to FIG. 7. In the

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sixth embodiment, only <u>different</u> aspects <u>different</u> from the fourth embodiment are described. Identical reference numerals to the fourth embodiment are applied to <u>substantially</u> the same of <u>eorresponding</u> members in the sixth embodiment, and <u>overlapped overlapping</u> description is omitted. Note that in the fourth embodiment the number of voids 32 is four.

Please replace the paragraph starting with "In the present embodiment" beginning on page 29, lines 4-13 with the following amended paragraph:

In the present embodiment, a first void element 32a is provided between the circumferential wall 25 and the stator core 16 by forming the recess 36 in the inner circumferential surface 25a of the circumferential wall 25. The recess 36 is formed by outwardly expanding a part of the elastic part 25d of the circumferential wall 25, which corresponds to the recess 36, in the radial direction of the stator core 16. A second void element 32b is also provided between the circumferential wall 25 and the stator core 16 by forming the recess 17 in the outer circumferential surface 16c of the stator core 16. Note that in the present embodiment, the thinned portion 17b of the first embodiment, which is shown in FIG. 2, is eliminated from the recess 17.

Please replace the paragraph starting with "As shown in Fig. 7" beginning on page 30, lines 3-12with the following amended paragraph:

As shown in FIG. 7, each void 32 adjoins two of the voids 32. Each void 32 is provided in such a manner that the void 32 and one <u>adjacent</u> of the voids 32, which is adjoined to the void 32, are approached to each other between the respective first void elements 32a. Therefore, each void 32 is provided in such a manner that the void 32 and the <u>other adjacent</u> void 32, which is adjoined to the void 32, are kept from each other by a relatively large distance in the circumferential direction of the stator core 16 between the first void elements 32a. Thereby, in the waved-shape of the circumferential wall 25 in the circumferential direction of the stator core 16, which is formed by the outward expansion of a plurality of the elastic parts 25d, a vertex of each wave is arranged at intervals of an unequal angle around the axis L.

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Please replace the paragraph starting with "(14) Each void 32" beginning on page 30, lines 18-22 and ending on page 31, lines 1-10 with the following amended paragraph:

(14) Each void 32 includes the first void element 32a, which is provided by the recess 36 formed by expanding the part of the elastic part 25d outwardly in the radial direction of the stator 16, and the second void element 32b, which is provided by forming the recess 17 in the outer circumferential surface 16c of the stator 16. Therefore, in order to fulfill a predetermined property of an elastic deformation of the elastic part 25d, the elastic part 25d as a whole does not require expanding outwardlyoutward expansion in the radial direction of the stator core 16. Thereby, for example, a demand is fulfilled for suppressing unevenness of a configuration of the electric type compressor, specifically, a demandand in particular for suppressing waves of the shape of the outer circumferential surface 25c of the circumferential wall 25—is fulfilled. In addition, the partial expansion of the circumferential wall 25 prevents the rigidity of the circumferential wall 25 from excessively being reducing—reduced by the outward expansion of the circumferential wall 25. Furthermore, the predetermined property of the elastic deformation of the elastic part 25d is fulfilledgained. Thus, appropriate tightening force is obtained.

Please replace the paragraph starting with "An electric type" beginning on page 31, lines 12-17 with the following amended paragraph:

An electric type compressor for a vehicle air conditioning apparatus according to a seventh preferred embodiment of the present invention will now be described with reference to FIG. 8. In the seventh embodiment, only different aspects different from the sixth embodiment are described. Identical reference numerals to the sixth embodiment are applied to substantially the same or corresponding members in the seventh embodiment, and overlapped overlapping description is omitted.

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Please replace the paragraph starting with "In the present embodiment" beginning on page 31, lines 19-22 and ending on page 32, lines 1-10 with the following amended paragraph:

In the present embodiment, a plurality of recesses 17 is set in such a manner that the length in the circumferential direction of some of the recesses 17 becomes is smaller than that of the other recesses 17. In FIG. 8, the number of the recesses 17, which is formed in the stator core 16, is four, and two of the recesses 17 inof the four recesses 17 are smaller in length in the circumferential direction than the two other two-recesses 17. Therefore, the protrusion 31 of the stator core 16, that is, or the contacting portion 33 between the circumferential wall 25 and the stator core 16 is arranged at intervals of an unequal angle around the axis L. Thereby, some of theadjacent pitches P between the contacting portions 33, which are located next to each other, is are different from the each other pitches P. In FIG. 8, pitches P1 are larger than pitches P2. In this case, in comparison with the elastic part 25d, whose pitch P1 between the contacting portions 33 is relatively large, it is more difficult that for the elastic part 25d, whose pitch P2 between the contacting portions 33 is relatively small, to elastically deforms.

Please replace the paragraph starting with "(15) A plurality of" beginning on page 32, lines 14-22 and ending on page 33, lines 1-6 with the following amended paragraph:

(15) A plurality of the recesses 32 is set in such a manner that the plurality of contacting portions 33 between the circumferential wall 25 and the stator core 16 is arranged at intervals of an unequal angle around the axis L. Therefore, if the circumferential wall 25 and the stator core 16 shrink so as to tightly fit each other due to thermal effects, an amount of elastic deformation of the plurality of elastic parts 25d becomes also unequal. In this case, however, in the plurality of elastic parts 25d, some of the elastic parts 25d have different spring constant from the other elastic parts 25d. Namely, some of the elastic parts 25d have a different natural frequency from the other elastic parts 25d. Therefore, the difference between the natural frequencies of the elastic parts 25d prevents all the elastic parts 25d from simultaneously resonating due to the vibration of the stator core 16. Thereby,

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the generation of the vibration and noise is reduced due to the resonance of in the electric type compressor eaused by the resonance is reduced.

Please replace the paragraphs starting with "In the present invention" beginning on page 33, lines 8-9-22 and starting with "In the above-described embodiments" beginning on page 33, lines 11-19 with the following amended paragraph:

In the present invention, following alternative embodiments are also practiced. In the above-described embodiments, the compressor housing 11 or the circumferential wall 25 is made of the aluminum and the stator core 16 is made of silicone steel, whose thermal expansion coefficient is different from that of the aluminum. In alternative embodiments to the above-described embodiments, the compressor housing 11, whose thermal expansion coefficient is different from the stator core 16, is made of metallic material other than the aluminum. For example, the compressor housing 11 is made of resin material.

In the above-described embodiments, the compressor housing 11 or the circumferential wall 25 is made of the aluminum and the stator core 16 is made of silicone steel, whose thermal expansion coefficient is different from that of the aluminum. In alternative embodiments to the above-described embodiments, the compressor housing 11, whose thermal expansion coefficient is different from the stator core 16, is made of metallic material other than the aluminum. For example, the compressor housing 11 is made of resin material.

Please replace the paragraph starting with "In the first embodiment" beginning on page 34, lines 18-22 and ending on page 28, lines 1-4 with the following amended paragraph:

In the first embodiment to-through the fifth embodiment, a plurality of the voids 32 is provided in such a manner that the contacting portions 33 between the circumferential wall 25 and the stator core 16 are arranged at intervals of an equal angle around the axis L. In alternative embodiments to the first embodiment through the fifth embodiment, the plurality of voids 32 is

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provided in such a manner that the contacting portions 33 between the circumferential wall 25 and the stator core 16 are arranged at intervals of an unequal angle around the axis L. In this case, the above-described effect (15) is substantially obtained.

Please replace the paragraph starting with "In the second embodiment" beginning on page 35, lines 5-8 with the following amended paragraph:

In the second embodiment to through the seventh embodiment, the coil 15 is distributively wound around the teeth 16b. In alternative embodiments to the second embodiment through the seventh embodiment, the coil 15 is intensively wound around the teeth 16b.

Please replace the paragraph starting with "In the sixth and seventh embodiments," beginning on page 35, lines 10-22 and ending on page 36, line 1 with the following amended paragraph:

In the sixth and seventh embodiments, the first void element 32a, which is provided by forming the recess 36 in the inner circumferential surface 25a of the circumferential wall 25, and the second void element 32b, which is provided by forming the recess 17 in the outer circumferential surface 16c of the stator core 16. The first and second void elements 32a and 32b are connected to each other in the radial direction of the stator core 16. Thereby, one void 32 is formed. In alternative embodiments to the sixth and seventh embodiments, however, the first void element 32a, which is provided by forming the recess 36 in the inner circumferential surface 25a of the circumferential wall 25, and the second void element 32b, which is provided by forming the recess 17 in the outer circumferential surface 16c of the stator core 16. The first and second void elements 32a and 32b are separated from each other in the radial direction of the stator core 16. Thereby, the first void element 32a and the second void element 32b are each individually formed. That is, in this case, the number of voids 32, which is provided around the axis L of the stator core 16, is eight.

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Please replace the paragraph starting with "Therefore, the present examples" beginning on page 36, lines 15-17 with the following amended paragraph:

Therefore, the present examples and embodiments are to be considered as illustrative and not restrictive, and the invention is not to be limited to the details given herein but may be modified within the scope of the appended claims.